# (NIR)

## Dynamic Studies of Small Animals with a Four-Color DOT Imager

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### ABSTRACT

introduce a four-wavelength dynamic optical tomography system for small animal studies. A cotaxic small animal measuring head was developed, which allows imaging of any body site of the mail. We present a setup for non-invisor dynamic optical imaging of the rat brain. The measuring d as well as the fiberoptics are compatible with in-magnet studies.

We give a detailed description of the implementation of the forer avordength capability and the way give a detailed description of constraints of the forer avordence of the series developed to series instrument functionality and that integrity for the device. Instrument performance managements that are advantated with the second ways and the second s

We present initial experimental results from dynamic optical measurements of the physiologic response of the rat brain to electric paws stimulation. The hemodynamic response in the brain for different stimulation sites is discussed. The results demonstrate excellent sensitivity of the instrument for measuring hemodynamics in small animal studies.

### INSTRUMENTATION

The instrument developed is based on the NIRx DYNOT imaging platform, which has been desin detail before [1,2]. Key features of the device inclusion ntinuous wave (cw) Diffuse Optical Tomographic (DOT) measurements @ 2- 75 fra second depending on number of sources

- Time division multiplexing of up to 32 sources (S)
- Parallel readout of up to 32 detectors (D)
- Parallel measurement of up to 5 u utexcurs (1/) Parallel measurement of up to four frequency-encoded wavelengths (WL) Dynamic detection range 1:10° (90 dB<sub>op</sub>) through source-synchronized detector gain switching
- Switching Current applications: Mammography, imaging of peripheral vasculature, functional brain imaging, small animal imaging.

### 1) HARDWARE

### wr-Wavelength Capabilit

- The following modifications were made to achieve simultaneous s four-color laser of Model 8000 laser diode controller (Newport Corp.) used in DYNOT accommodates modules for independent control of up to four thermo-electrically cooled laser diodes.
- Lasers used: 725 nm (250 mWmax), 760 nm, 810 nm, 860 nm (all 400 mWmax) Lasers are mounted in compact "sandwich" configuration to save space and to allow efficient forced air cooling with fan.
- DYNOT standard power supply can be used without modification
- The optical switch (OS) is identical in design and function to the device in the previously described dual-wavelength imager [1]. Four-color operation of the OS was achieved by developing a new incoupling optics with the following features (see Fig. 1):
- Four-wavelength mixer/incoupler combines and focuses laser beams into optical switch. · Custom made dichroic mirrors (Omega Optical, Inc.) allow efficient (90% typ.) wavelength
- Laser delivery fibers and the dichroic mirrors are individually adjustable (translation, tilt) to achieve optimum beam collinearity and centricity with respect to the OS.
- DYNOT programmable multi-channel optical detector (PMOD) is designed to allow simultaneous ction of up to four frequency-encoded optical signals. The following upgrades to the detection side detection of up to four frequency-encoded optical signals. of the system were performed for four-wavelength operatio
- A second lock-in module was added to each of the 32 detector channel boards to upgrade from dual- to quad-wavelength detection.
- A second phase shifter module was installed into the PMOD to condition the two additional reference signals for lock-in detection
- To acquire data from up to 128 measurement channels (= 4 WL × 32 detectors), a second 64-channel data acquisition (DAQ) board (National Instruments PCI6033E) was installed into the control PC.
- A new interface board was developed for the PMOD that accommodates connections to the two DAQ boards.

### atible Small Animal Imaging Head

- The following hardware developments make the instrument compatible with in-magnet studies 12 feet long fiber optic cables used for light transmission between instrument and target to keep instrument in safe distance from magnet.
- substance from magnet.

  Illumination bundle disance r = 0.8 mm , detection bundle diameter 1.0 mm, probe end diameter = 2.0 mm
- No metal components used in fiber optics (plastic probe ferrules)
- · No metal components used in animal holder
- An imaging head was designed to ensure stable position of the animal and good optical probe contact (see Fig. 2).
- Stereotaxic positioning of the animal using ear bars and bite bar
- Fiber holder allows high-density arrangement of probes (3-mm center-to-center spacing) Foam cushion in fiber holder allows easy adjustment of probe pressure
- ecial mouth piece bends 30° upward to make contact with roof of the mo
- · Fiber probes integrated into ear bars

### 2) SOFTWARE

- 2) NUT WARE The DNNOT control software is implemented in the LabVEW language (National Instruments, Inc.) and has been described in detail before for the case of four workedge data service and a service of the case of four workedge data service for all source-detector pairs to programe the instrument of a measurement. Contains "Setup Cases" of the case of the measurement of the case of the workedge data service for all source-detector pairs to programe the instrument of a measurement. Contains "Setup Cases" of the cases of pairs are cases of the measurement contains "Setup Cases" of pairs of the cases of pairs are cases of pairs are cases of pairs of the cases of pairs are cases.
  - Measurement Screen: Displays raw data in real time for all wavelengths.
  - System Checkend Servers: Contains a variety of automated or semi-automated data and hardware integrity checks, including: Detector dark noise measurement
  - · Optical alignment tools for the optical switch

- DATA INTEGRITY AND PERFORMANCE CHECK PROCEDURES
- Because the imaging problem is ill-posed and under-determined, it is of param importance that data collection be performed with the highest precision and accuracy poss acy possible Requires all hardware components to be intact and to perform according to specified quality standards.
  - Requires proper setup of optical measurement( e.g., appropriate gain settings, good probe-tissue contact).
- Large number of data channels (i.e., up to 32S × 32D × 4 WL = 4096 channels) requires:
- Automated or semi-automated test procedures to reduce test time and to increase reliability. · Easy-to-read visualization of complex results

### 1) GAIN SETTING

Gain settings for each S-D pair need to be established before each measurement. Channels with improper gain setup may experience excessive noise or signal saturation/distortion. Several methods of proper gain setup may expo ing the gain setup exist:

- Gain settings for each S-D pair are displayed in a color-contour plot (see Fig. 3A). Deviations from application-characteristic pattern is indicative of inappropriate gain setting.
- Because of the reciprocity of light transport, gains for reciprocal 8 D channels, (i.e.  $S_{i\mu} D_{i\mu}$ vs.  $S_{i\nu} D_{i\mu}$  are expected to be similar. For each S-D pair, the difference in gain for its reciprocal pair is calculated and displayed in a color-model contour plot. A difference greater than one gain step is indicative of inappropriate setup (Fig. 3B).

### 2) CORRELATION ANALYSIS

- For a time series of data, the correlation coefficient r between reciprocal S-D pairs is computed and graphed in a color contour plot.
- Non-random variation of physiologic data leads to high correlation values for recip channels with high signal-to-noise ratio (Fig. 4A). Data are low-pass filtered to mitigate the influence of random detection noise (Fig. 4B)
- Isolated low r values are indicative of bad fiber-tissue contact



Fig. 1. Optical switch with



### Fig. 2. Sterectavic rat imaging stage. A: Detailed view of the imaging assimal in the draine and element of entirel fibers on the head



Fig. 3. System setup checks: A: Color enco encoded display of differences between gain (not shown) is infractive of faulty setup.



## Fig. 4. Correlation values for physiologic time series of reciprocal channels. Strong positive correlation (values greater 0.8) are expected for reciprocal pairs not showing noise-dominated readings. A: Unfiltered result. B Correlation result after low-position filtering the data. Note the increased r values in the lower left compared to A.



sign







 $\frac{r_{i,j+j}}{r_{i,j+c}} \frac{r_{i+j+c,j+c}}{r_{i+j+c,j+j}} = \frac{s_i m_j d_{i+j}}{s_i m_i d_{i+c}} \frac{s_{i+j+c} m_j d_{i+c}}{s_{i+j+c} m_i d_{i+j}} = \frac{m_j}{m_c} = m_j^*$ 

### INSTRUMENT PERFORMANCE

- Dark noise test of detector electronics
  - · Detection of: · Component failure/aging in PMOD,
    - Problems with DAQ electronics
    - · Deterioration of grounding connections, shielding
    - External sources of EM interferences
- · Dark current is measured for each channel dependent on gain settings Display of noise level (STD) and noise power spectrum. 2) Illumination noise/stability
  - ion noise and drift is caused by
  - Laser instabilities
  - Typically long term (~sec m
  - · Minimized by TEC control of laser operating temperature Corrected by monitoring laser output power
  - · Variation of the incoupling efficiency of the OS
  - · Long term: thermal effects (heating of OS motor)
- Short term: Frame-to-frame variations in illumination strength due to repeatability limits of the mechanical beam-steering mechanism. Figs. 5-7 illustrate the measured noise and drift performance of the instrument



For equidistant placement of the probes along the perimeter of a cylindrical plantom (see  $\frac{1}{100}$ ,  $\mathbb{R}$ ), the measured signals can be modeled by matrix equation  $\mathbb{R}$ -SMD. ( $\mathbb{R}$  matrix of the measured readings,  $\mathbb{M}$ : matrix containing the fraction of intensity transmitted from St to JJ through the medium,  $\mathbb{R}$ ,  $\mathbb{D}$ : Matrices of source strength coefficients and detector sensitivity factors, respectively.)

For a circular geometry, the symmetry of **M** can be used to obtain estimates of the entries *m* of a matrix  $\mathbf{M} = a \mathbf{M}$ .

By creating the ratio  $r_i/m'_{ij} = a s_i d_j$  and dividing each resulting element by its row sum, a number proportional to  $d_i$  is obtained:  $d'_i = m d_i$ . Likewise, dividing elements  $a s_i d_j$  by their column sum yields estimates of the source strength coefficients  $s'_i = n s_i$ . An electronic calibration was implemented to account for relative inter-channel variation of the detector gain settings.

FOUR-COLOR OPTICAL IMAGING OF THE RAT BRAIN

· 31 fiber optic probes were placed on the head as schematically indicated in Fig. 10:

A male rat (approx. 400 g) was anesthetized, intubated, and positioned in the stereotaxic imaging head as seen in  $\frac{Fig.~2}{2}$ .

28 probes (note the product of the function and performance on the top of the head in a five-by-six rectangular grid with two corner positions left unoccupied.
 Two probes (nos. 29, 30) were placed in the ears.

 After instrument setup, a baseline measurement was performed for the duration of 1300 frames (~ 12 min) transact('1 kmm) The baseline measurement was followed by electric stimulation of each of the four paws in the order right hind, left findt, left front, right front. Each paw was stimulated in site cpochs which were applied every 150 imaging frames (?9.3), with each epoch lasting six imaging frames (~3 s). Stimulation was performed with 5 mA ac current (10 Hz).

Coefficients of variation (CV) were computed for all channels, and channels having CV values larger than 15% were excluded from further processing.

Raw data in the remaining channels were corrected for variations in laser power, which is monitored during the experiment.

· Data are subjected to an adaptive median filter to remove instantaneous negative spikes

The weight matrix was computed using a finite element model (FEM) to numerically solve the diffusion equation. The FEM mesh (shown in Fig. 10) representing the anatomy of the rat head was adapted from [4]. For the current calculations, an optically homogeneous model was used.

Truncated singular value decomposition (SVD) is used to solve the linear perturbation equation [6].

The reconstructed absorption coefficient images were used to compute image time series for oxygenated, deoxygenated, and total hemoglobin (Hboxy, Hbred, Hbtot, respectively) concentration changes.

A general linear model (GLM) algorithm [7] was used to find the best fit of each image node time series to a linear combination of four model functions, as schematically illustrated in Fig. 11.

The four model functions used were a constant (offset) term, linear and quadratic baseline drift functions, and a two-state boxcar function representing the idealized hemodynamic response of the brain to the stimulation.

The boxcar function was generated to reflect the periods of brain activation as determined from the raw spatial-averaged detector time series

The GLM coefficients for the boxcar function yield a representation of the spatially varying hemodynamic response to the stimulation.

No averaging over multiple epochs was performed for the analysis

Fig. 12 shows the spatial average of the reconstructed image time series for the three Hb states during three consecutive stimulation epochs of the left front paw. Onset and cessation of each epoch are

Hboxy concentration shows *increase* during stimulation: • Immediate rise (within one time frame = 0.5 s) at the beginning of stimulus. Steady increase during stimulation, peaking at the end of epoch. • Return to baseline starts immediately at end of epoch, return time  $\approx$  rise time.

Hbtot concentration shows biphasic behavior:
 Immediate rise (within one time frame  $\approx 0.5$  s) at epoch start.
 Peaking after 4-5 frames ( $\approx 0.25$  s).
 Undershoot of baseline following stimulation.

Therefore concerning to the second se

Fig. 13 shows spatial maps of the GLM coefficients for the boxcar model function computed on the reconstructed image time series for Hboxy and Hbred. The Hbred/Hboxy changes during stimulation occur primarily in a central region of the head that coincides with the location of the cortex. Some Hbred response can be seen in the outer regions of the head.

Classic somatosensory activation is expected to be centralized for hind paw stimulation and lateralized for front paw stimulation. Right side stimulation is expected to activate the left portion of the cortex, and vice versa. Some spatial variation of the roppose to different stimulation sites – mostly in the cutent of the response – is seen, but a clear somatosensory localization cannot be conclusively demonstrated.

To gain a more quantitative understanding of the spatial extent of activation, we calculated the cumulative sum of image nodes showing a given change in Hb state (Fig. 14). The results show significant variation in the activated brain region for different stimulation sites.

We presented data demonstrating the short and long term precision of the newly developed rat imager. Physiologic time series results show excellent measurement sensitivity to event related changes in Hb states in the rat brain.

We demonstrated the capability of measuring individual activation epochs with high repeatability and signal quality allowing analysis of individual events without the requirement of averaging over multiple epochs.

The stimulation parameters such as amplitude and duration need to be explored further.

We plan the refinement of the analysis. Possible strategies include the the use of more sophisticated model functions, the reconstruction of temporal features (such as delay times), the application of rate analysis, and the introduction of a more accurate optical model of the rat head.

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REFERENCES

CONCLUSION

A phantom based calibration protocol and calibration results were presented.

We proposed the following next steps to observe somato in the reconstruction results:

· Image reconstruction was achieved using the Normalized-Difference Method [5].

For each channel, readings were normalized to the temporal mean value during the initial baseline period.

For a symmetric medium, M is always a constant-diagonal (TOEPLITZ) matrix

Fig. 9 shows calibration results for the 4-WL imager

· One probe was places inside the mouth.

analysis and image reconstru-

1. Data pre-processing:

2 Image reconstruction

3. Post-processing

2) RESULTS

) METHODS

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9. Calibration results for 4-wavelength image. A: a coefficients for tour catestaton measurements performed and the second of the second se



Fig. 10. Mesh used for modeling light to (bottom) view. B: coronal (front) view.



Fig. 11. Schematic illustration of the action of a GLM



Fig. 12. Three series of the spatially averaged imaging results for the three Ho states. Shown are three consecutive spochs of hit from pass simulation for averaging over multiple spochs), holicotaid are series and and of stimulation spochs. An early increase in Hoory can be seen, followed by a delivered secresses in Hourd. The rise in Hoory ends at the recording of the similar, while Heard shows delayed panking. A biparticle Hoter segments or toberwid.



## Fig. 13. GLM results for the reconstructed image time series for Hboay (A) and Hintel (B). Shown are spatial maps of the GLM coefficients for the board function representing particults of brain activation as estimated from the spatial the activator area of more signly as adoption of the foreface with the back. Another solution based the none.



A phantom measurement based calibration procedure has been introduced before, which allows determination of the relative inter-channel variation of the imager [3]:

For a symmetric phantom, the light intensity transmitted from a source to a detector depends only on S - D separation (see Fig. 8)

tony on  $s' \to Separaton (see <u>rig. a)</u>$ Deviations in the measured readings for different SD pairs having the same probe separationcan be attributed to instrumentation influences. These are numerically separated into $differences in source strength scenes, or <math>\leq ad \leq 1$ ) and differences in detector sensitivity (expressed in source strength factors,  $0 \leq ad \leq 1$ ).

3) Calibration protocol